

# Physics-Infused Differential-Algebraic Reduced-Order Models for Multi-Disciplinary Systems

Carlos Vargas Venagas and **Dan**ing Huang

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**PennState**  
College of Engineering

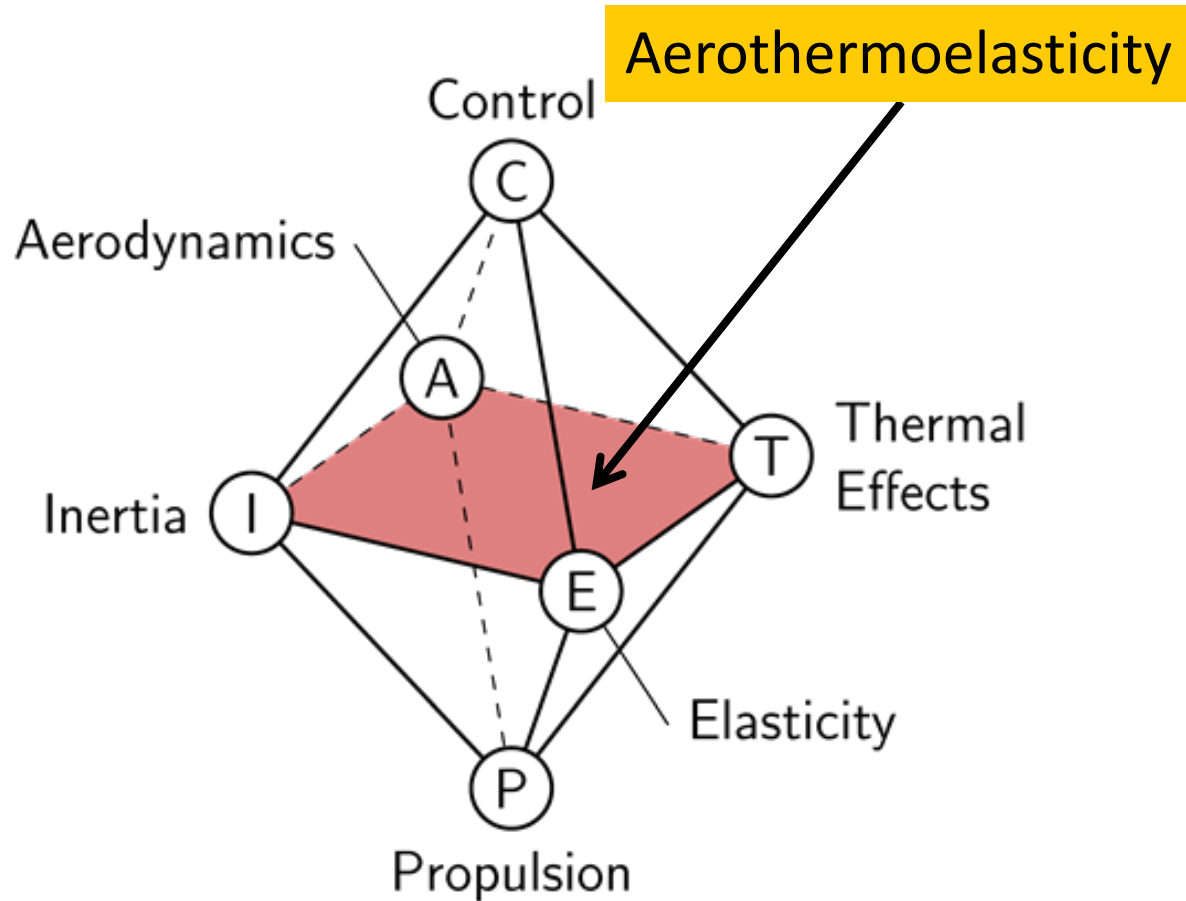
**APUS Lab**

Aerospace multi-Physical and  
Unconventional Systems

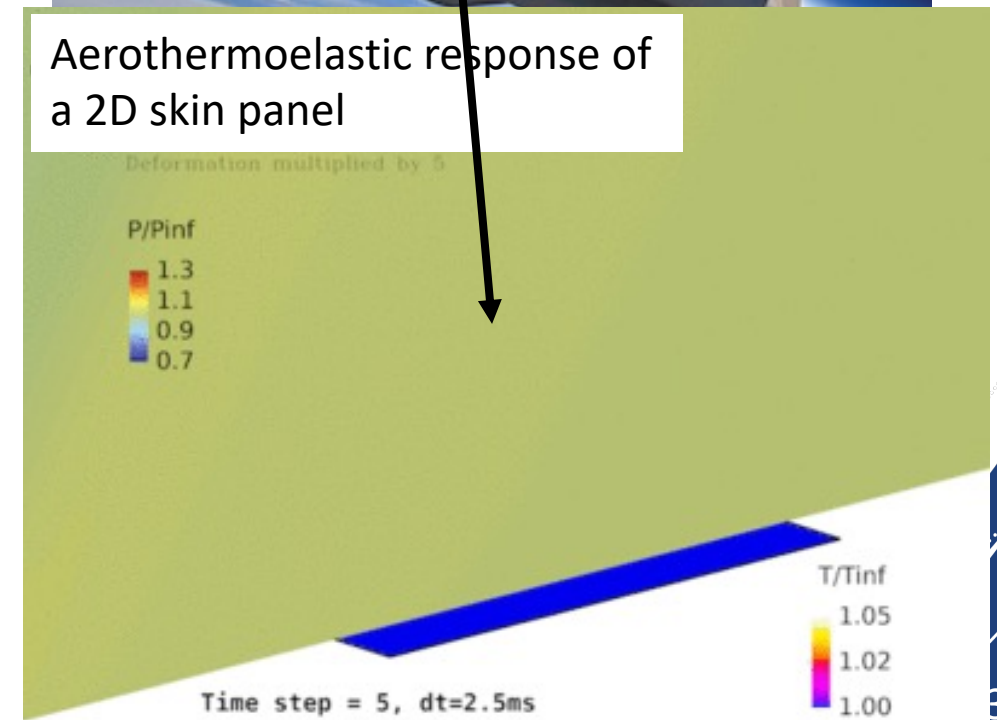
# Background

Hypersonic Aerothermoelasticity

# Barrier to fly at Hypersonic speed

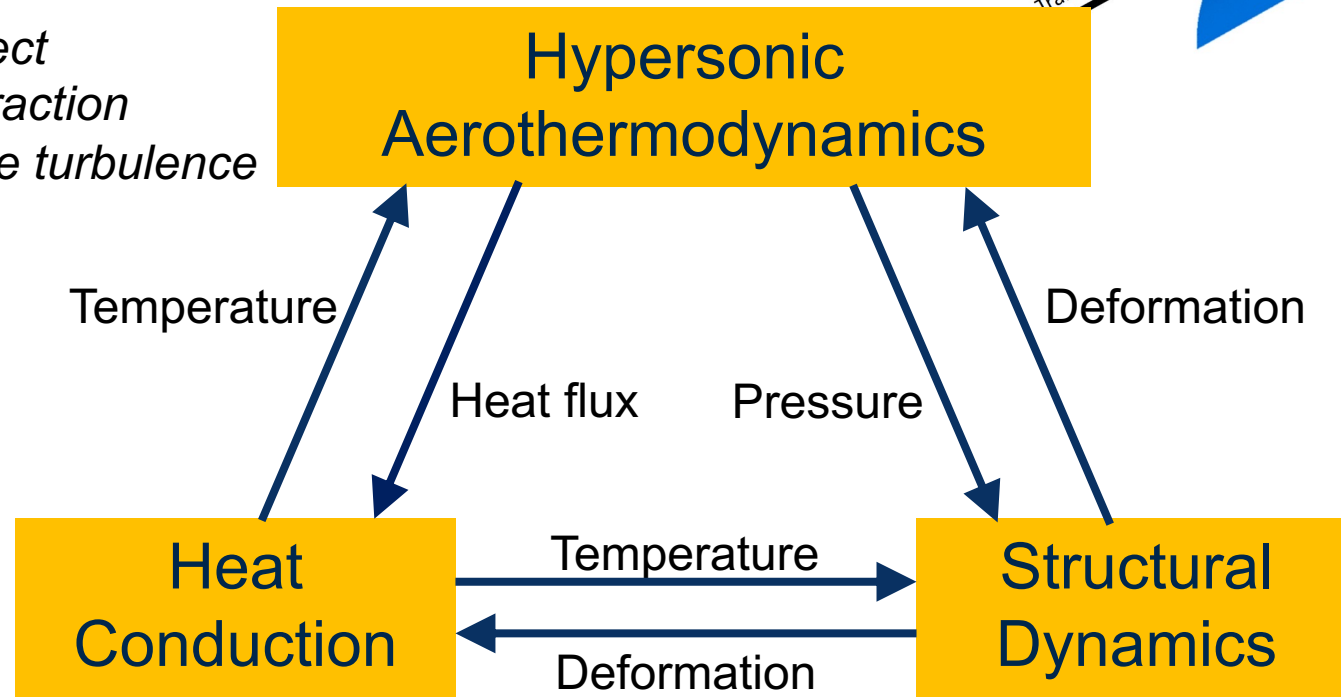
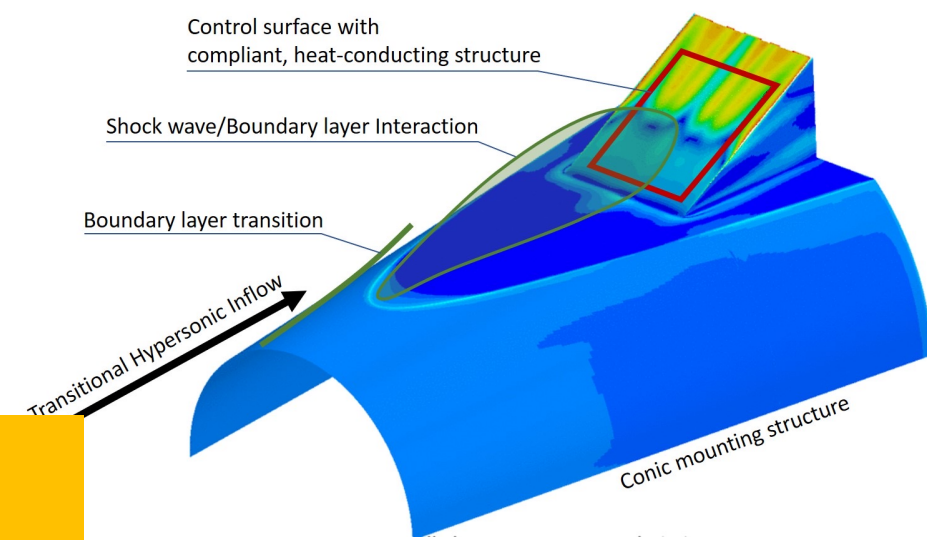


Aerothermoelastic response of a 2D skin panel



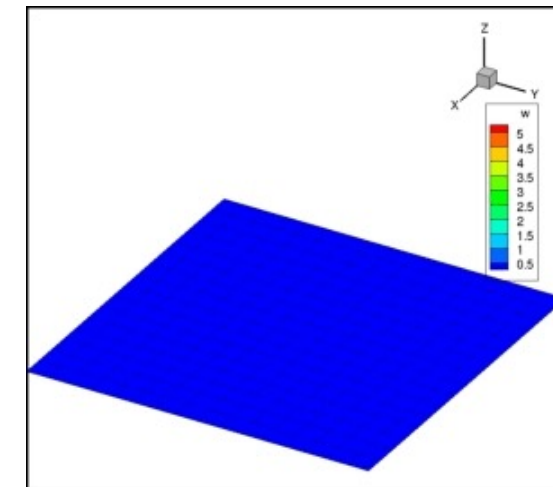
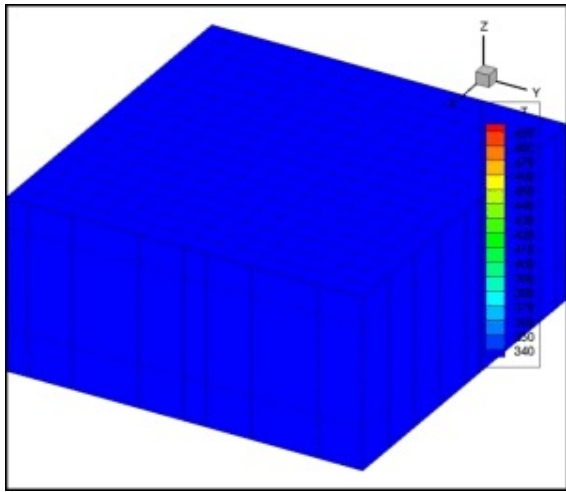
# As a Multi-disciplinary system

- *Real gas effect*
- *Viscous interaction*
- *Compressible turbulence*



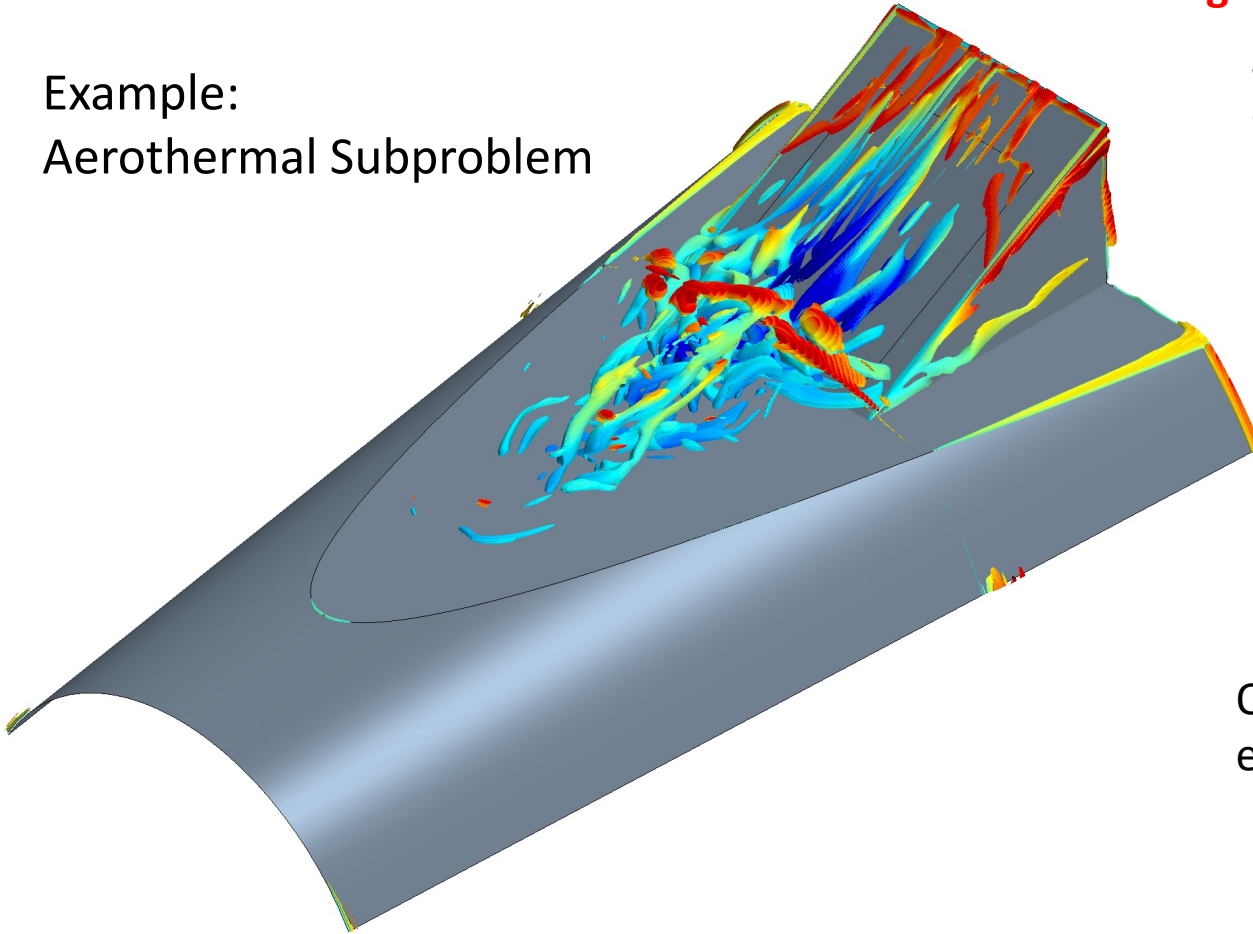
- *Thermal management*
- *Material degradation*
- *Charring and ablation*

- *Flutter and buckling*
- *Fatigue and creep*
- *Reliability assessment*



# Challenge to analyze, optimize, control such systems...

Example:  
Aerothermal Subproblem



**High computational cost**

States  $>10^9$   
e.g. flow states

**Vast design space**

Parameters  $\sim 10^3$   
e.g. geometrical configuration

$$\dot{x} = f(\boxed{x}, u; \boxed{\mu})$$

$$\boxed{z} = h(x, \boxed{u}; \mu)$$

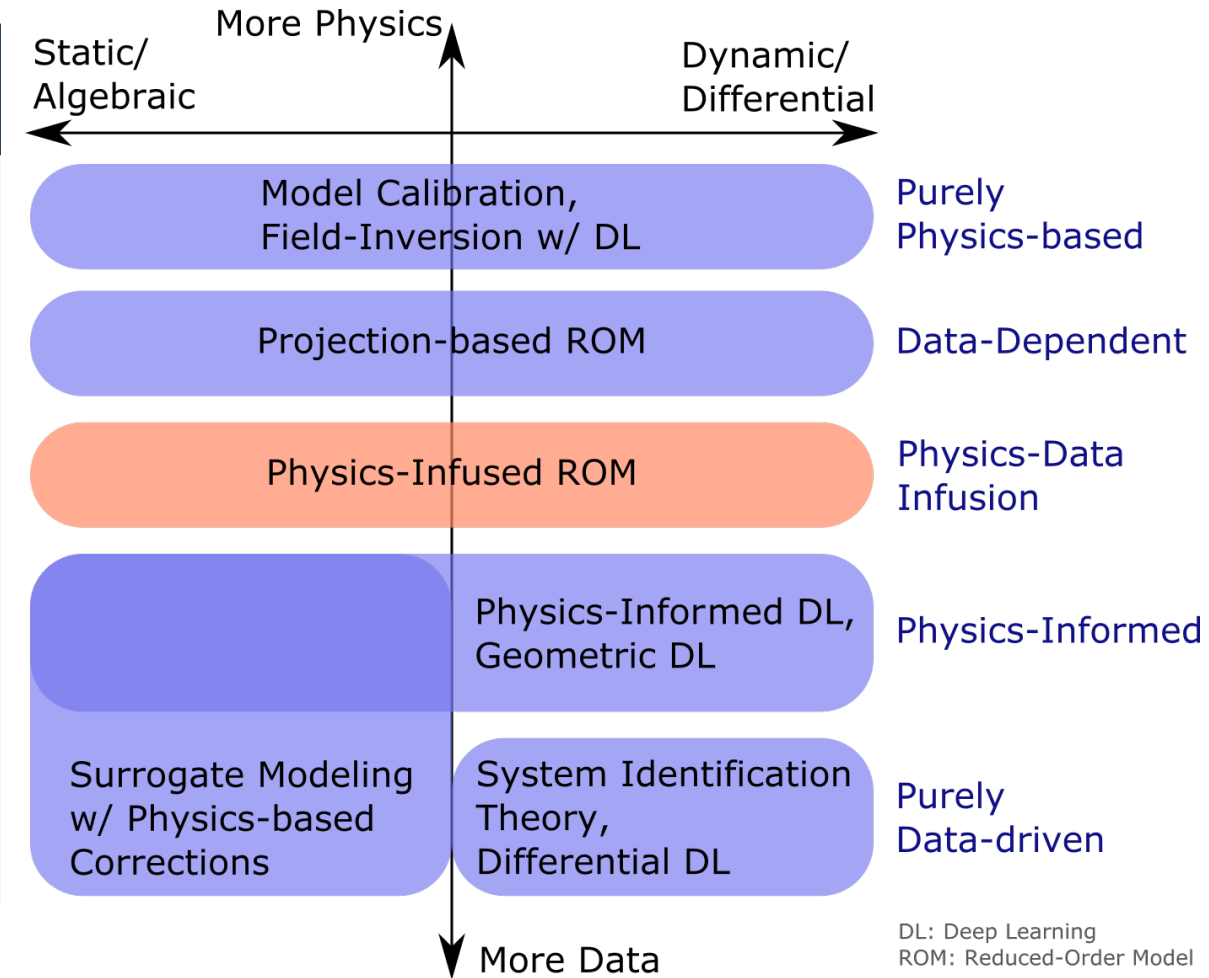
Output  $\sim 10^3$   
e.g. aerothermal loads

Input  $\sim 10^3$   
e.g. thermoelastic response,  
control commands

**High-dimensional  
optimal control laws &  
uncertainty quantification**

# What are the options?

Functional form of predictive model	Generalizability to system parameters	Computational cost
Physics (+ Data)	High	High
Physics	Mid	Mid
Physics + Data	High?	Low?
Data	Mid	Low
Data	Low	Low



# Formulation

Physics-Infused Reduced-Order Modeling

# General Idea

Examples	Boundary layer	Slender structure
Full-order	Navier-Stokes Eqn.	Elasticity Eqns.
States	Density, velocity, energy	3D displacement field
Low-order	Momentum integral Eqn.	Euler-Bernoulli Eqn.
State variables	BL thicknesses	1D disp. field
Aux. variables	Shape factor, Skin friction	Bending stiffness

- Full-Order Model (FOM)

$$\dot{\mathbf{x}} = \mathbf{F}(\mathbf{x}, \mathbf{u}; \boldsymbol{\mu})$$

$$\mathbf{z} = \mathbf{H}(\mathbf{x}, \mathbf{u}; \boldsymbol{\mu})$$

- Low-Order Model – *First principle, much less states*

$$0 = \mathbf{f}(\mathbf{y}, \dot{\mathbf{y}}, \mathbf{c}, \mathbf{u}; \boldsymbol{\mu}) \quad \leftarrow \text{Differential-algebraic Eqn.}$$

$$\mathbf{c} = \mathbf{g}(\mathbf{y}, \mathbf{u}; \boldsymbol{\mu}) \quad \leftarrow \text{Auxiliary variables}$$

$$\mathbf{z} = \mathbf{h}(\mathbf{y}, \mathbf{c}, \mathbf{u}; \boldsymbol{\mu})$$

- Physics-Infused Reduced-Order Model

$$0 = \mathbf{f}(\mathbf{y}, \dot{\mathbf{y}}, \mathbf{c}, \mathbf{u}; \boldsymbol{\mu})$$

$$\mathbf{A}\dot{\mathbf{c}} = \tilde{\mathbf{g}}(\mathbf{y}, \mathbf{u}, \mathbf{c}; \boldsymbol{\mu}) \quad \leftarrow \text{Augmented form}$$

$$\mathbf{z} = \mathbf{h}(\mathbf{y}, \mathbf{c}, \mathbf{u}; \boldsymbol{\mu})$$

- DAE-constrained optimization

$$\mathbf{A}^*, \boldsymbol{\Theta}^* = \underset{\mathbf{A}, \boldsymbol{\Theta}}{\operatorname{argmin}} \|\mathbf{z}_{FOM} - \mathbf{z}\|$$

$$\text{s.t. } 0 = \mathbf{f}(\mathbf{y}, \dot{\mathbf{y}}, \mathbf{c}, \mathbf{u}; \boldsymbol{\mu})$$

$$\mathbf{A}\dot{\mathbf{c}} = \tilde{\mathbf{g}}(\mathbf{y}, \mathbf{u}, \mathbf{c}; \boldsymbol{\mu}; \boldsymbol{\Theta})$$

$$\mathbf{z} = \mathbf{h}(\mathbf{y}, \mathbf{c}, \mathbf{u}; \boldsymbol{\mu})$$

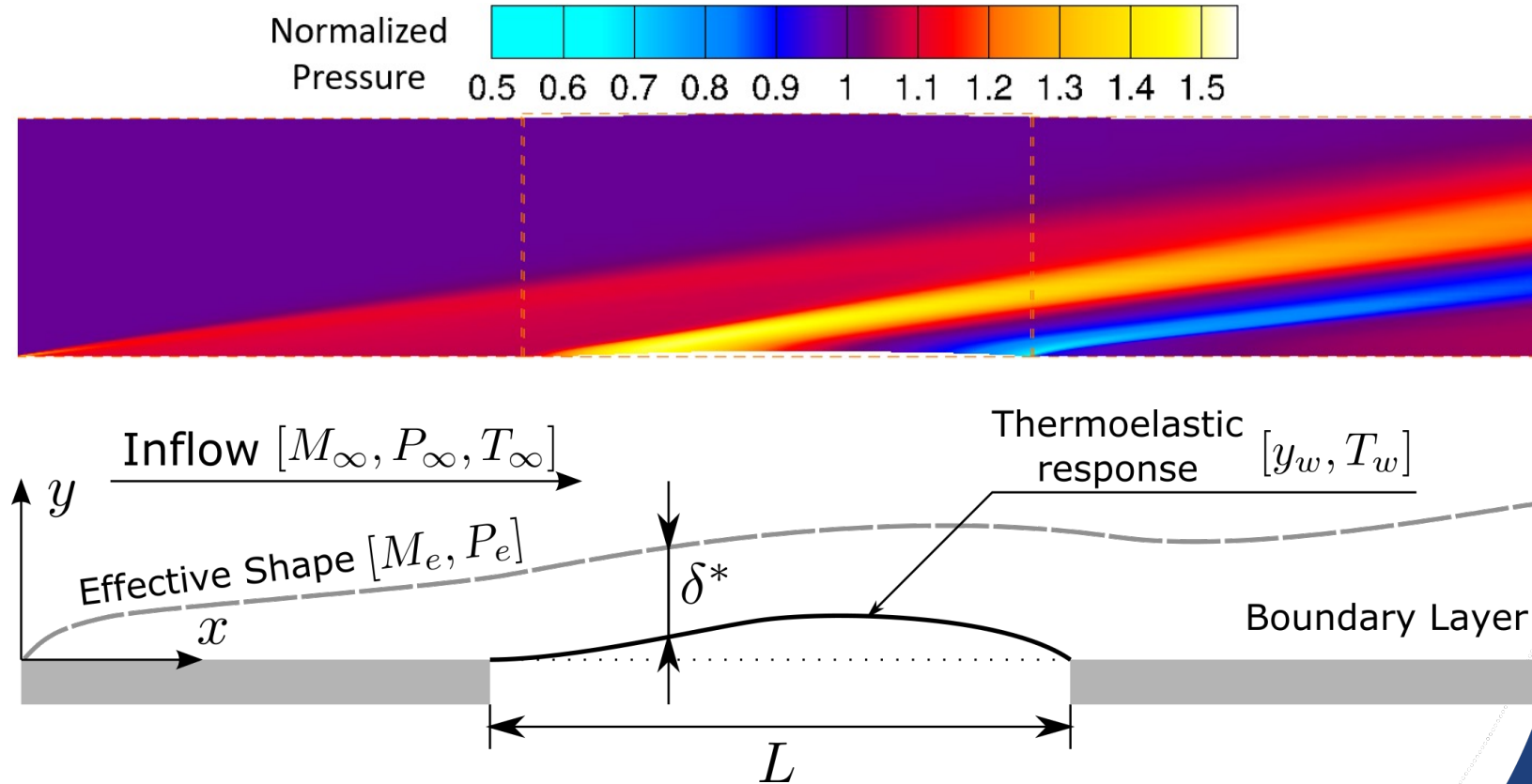


# Back to Hypersonic aerothermodynamics

## First-principle modeling: Turbulence Viscous-Inviscid Interaction (TVI)

$$\begin{cases} \frac{d}{dx} \left( \frac{\delta^*}{H} \right) + \left( H_i \frac{T_w}{T_o} - 4 \right) \frac{\delta^*}{HM_e} \frac{dM_e}{dx} = \frac{C_f}{2} \\ p_e(x) = p_\infty \left( 1 + \frac{\gamma - 1}{2} M_\infty^2 \frac{dy_e}{dx} \right)^{\frac{2\gamma}{\gamma - 1}} \\ y_e = y_w + \delta^* \end{cases}$$

- Classical integral equations that respect physics
- A system of differential-algebraic equations (DAEs)
- But misses some physics, e.g. High-temperature effects



# Casting to state-space form

## First-principle modeling: Turbulence Viscous-Inviscid Interaction (TVI)

$$\mathbf{M}(\mathbf{y}, \mathbf{c}; \tau) \frac{d\mathbf{y}}{dx} = \mathbf{f}(\mathbf{y}, \mathbf{c}, x; \mathbf{u}, \tau)$$

$$\mathbf{c} = \mathbf{g}(\mathbf{y}, x; \mathbf{u}, \tau)$$

$$\mathbf{z} = \mathbf{h}(\mathbf{y}, \mathbf{c}, x; \mathbf{u}, \tau)$$

- Classical integral equations that respect physics
- A system of differential-algebraic equations (DAEs)
- But misses some physics, e.g. High-temperature effects

$$\mathbf{M}(\mathbf{y}, \mathbf{c}; \tau) = \begin{bmatrix} H & \alpha \frac{H\delta^*}{M_e} - 2\delta^* M_e \xi & 0 \\ M_e & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad \mathbf{f}(\mathbf{y}, \mathbf{c}, x; \mathbf{u}, \tau) = \begin{bmatrix} H^2 \frac{C_f}{2} \\ \alpha - \frac{dy_w}{dx} \\ P_e - P_o \left(1 + \frac{\gamma-1}{2} M_e^2\right)^{\frac{-\gamma}{\gamma-1}} \end{bmatrix}$$

Aux. variables:

- Shape factor
- Skin friction coefficient
- Pressure ratio

$$\mathbf{g}(\mathbf{y}, x; \mathbf{u}, \tau) = \begin{bmatrix} \frac{\gamma-1}{2} M_e(x)^2 \left(1 + H_i \frac{T_w(x)}{T_o}\right) \\ 0.026 \frac{T_e}{T^*} \left(\frac{\rho_\infty \mu^*}{\rho_e \mu_e}\right)^{1/4} Re_\theta^{-1/4} \\ 1 \end{bmatrix}$$

Output variables:

- Surface pressure
- Surface heat flux

$$\mathbf{h}(\mathbf{y}, \mathbf{c}, x; \mathbf{u}, \tau) = \begin{bmatrix} k_p P_e \\ \frac{C_f}{2Pr^{2/3}} \rho u_e [h_{aw}(T_r) - h(T_w)] \end{bmatrix}$$

# Creating the PIRO model

## First-principle modeling: Turbulence Viscous-Inviscid Interaction (TVI)

$$\mathbf{M}(\mathbf{y}, \mathbf{c}; \tau) \frac{d\mathbf{y}}{dx} = \mathbf{f}(\mathbf{y}, \mathbf{c}, x; \mathbf{u}, \tau)$$

$$\mathbf{c} = \mathbf{g}(\mathbf{y}, x; \mathbf{u}, \tau)$$

$$\mathbf{z} = \mathbf{h}(\mathbf{y}, \mathbf{c}, x; \mathbf{u}, \tau)$$

- Classical integral equations that respect physics
- A system of differential-algebraic equations (DAEs)
- But misses some physics, e.g. High-temperature effects

## Model augmentation by functional correction

$$\mathbf{M}(\mathbf{y}, \mathbf{c}; \tau) \frac{d\mathbf{y}}{dx} = \mathbf{f}(\mathbf{y}, \mathbf{c}, x; \mathbf{u}, \tau)$$

$$\mathbf{c} = \beta(\mathbf{y}, x; \mathbf{u}, \tau) \odot \mathbf{g}(\mathbf{y}, x; \mathbf{u}, \tau)$$

$$\mathbf{z} = \mathbf{h}(\mathbf{y}, \mathbf{c}, x; \mathbf{u}, \tau)$$

- To account for missing physics -
- Taking an algebraic multiplicative form
- A new DAE with **unknown functions**

## Learn unknown functionals from data

$$\mathbf{B}^i = \arg \min_{\mathbf{B}} J(\mathbf{z}_{RANS}^i, \mathbf{z}(\mathbf{B}))$$

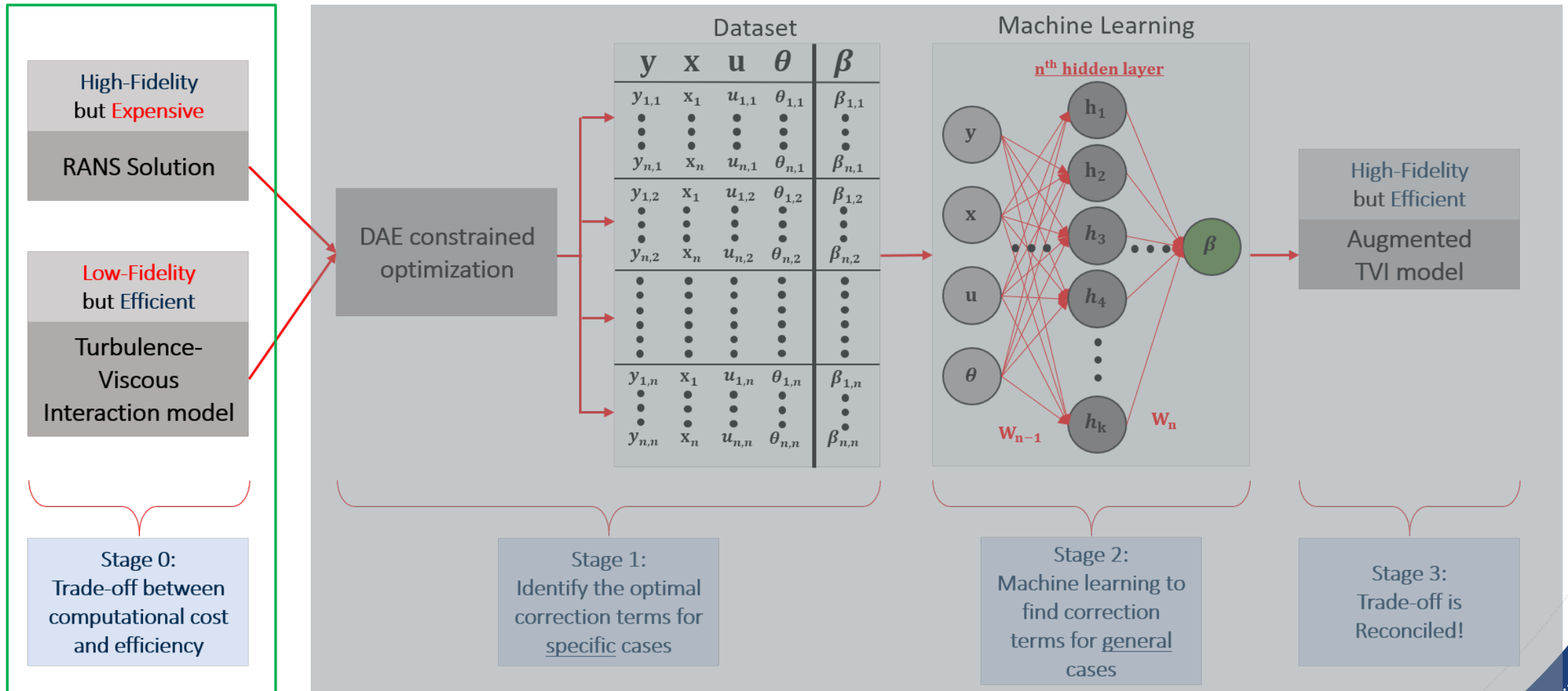
$$s.t. \quad \mathbf{M}(\mathbf{y}, \mathbf{c}; \tau) \frac{d\mathbf{y}}{dx} = \mathbf{f}(\mathbf{y}, \mathbf{c}, x; \mathbf{u}, \tau)$$

$$\mathbf{c} = \beta_{spl}(x; \mathbf{B}) \odot \mathbf{g}(\mathbf{y}, x; \mathbf{u}, \tau)$$

$$\mathbf{z} = \mathbf{h}(\mathbf{y}, \mathbf{c}, x; \mathbf{u}, \tau)$$

- Learn corrections by a DAE-constrained optimization
- Works for computational (RANS/LES/DNS) or experimental data
- Captures more physics and is interpretable!

# Methodology Overview



# Stage 0: RANS Solutions

Normalized  
Pressure



Flow conditions

Thermoelastic  
Response

Computational  
Grid

1.0 m

1.0 m

1.0 m

0.5 m

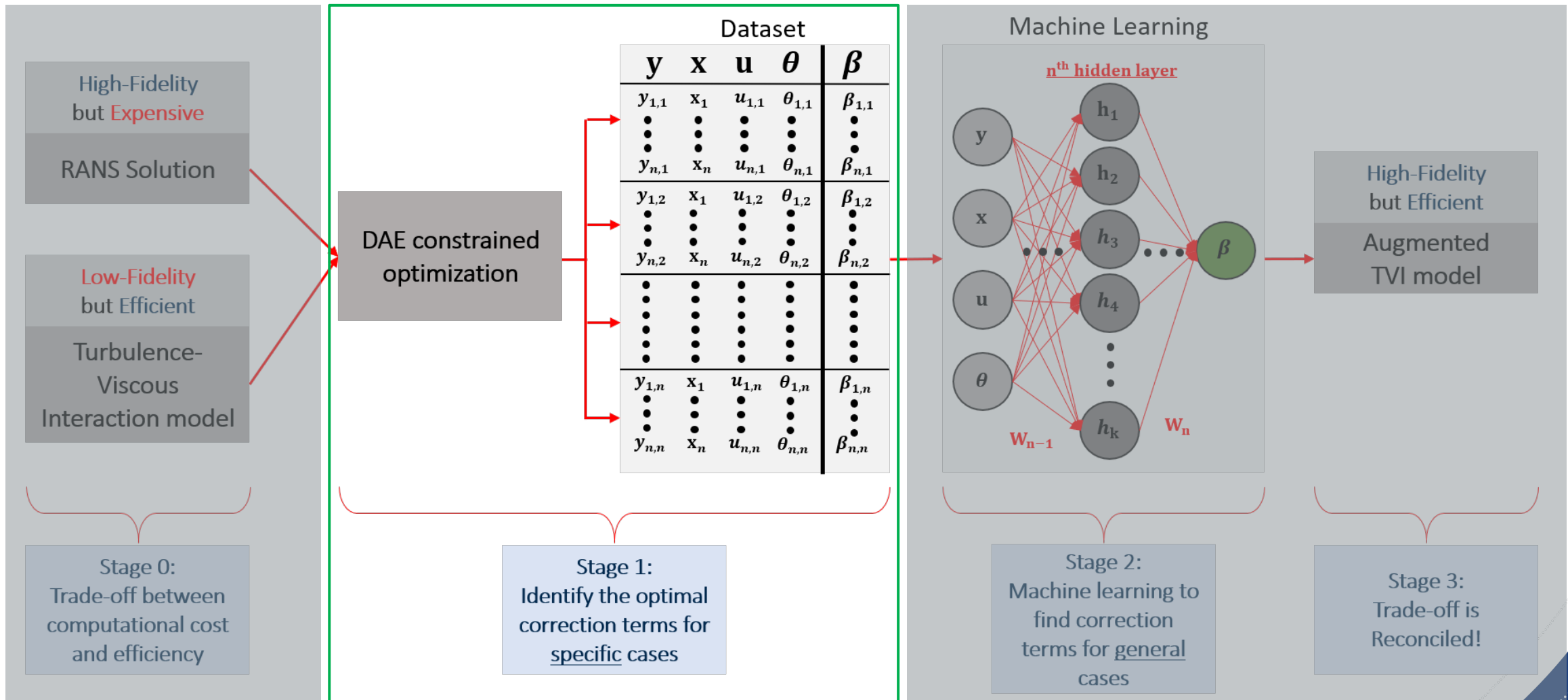
Front  
Domain

Panel  
Domain

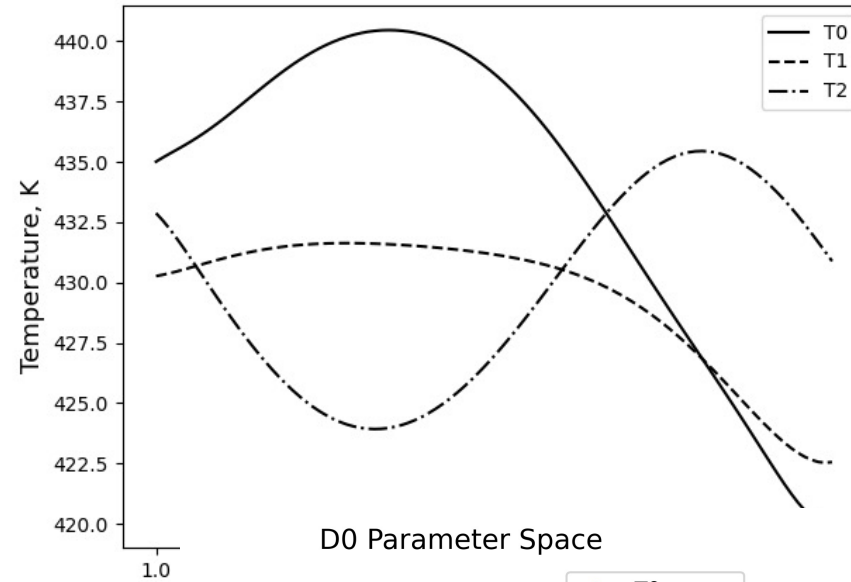
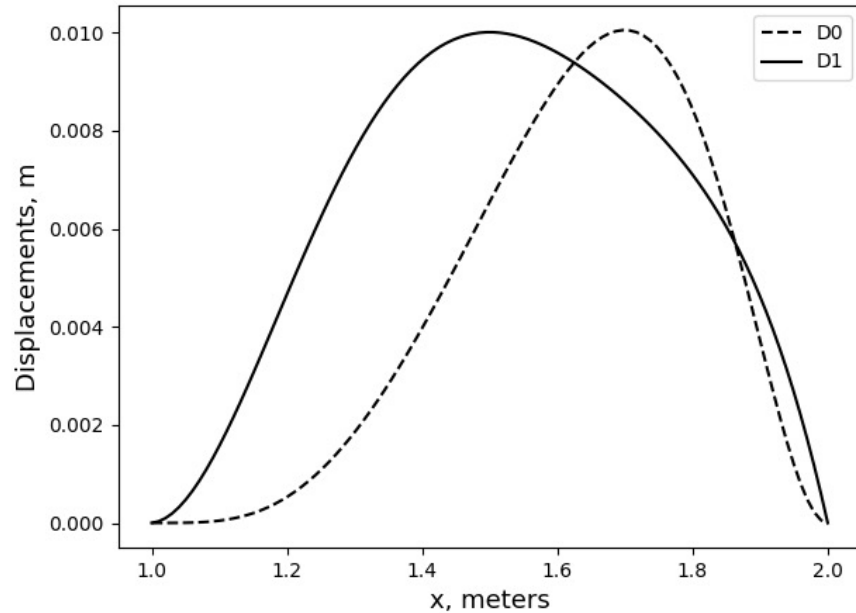
Rear  
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# Stage 1: Solving Inverse Problems

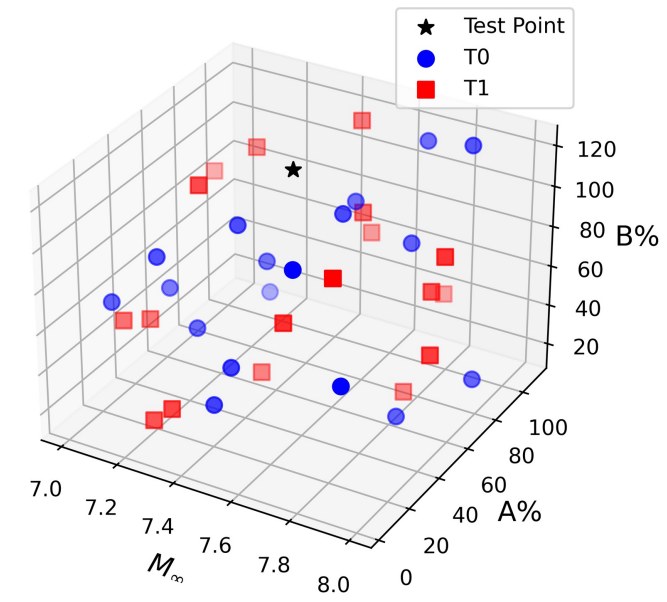
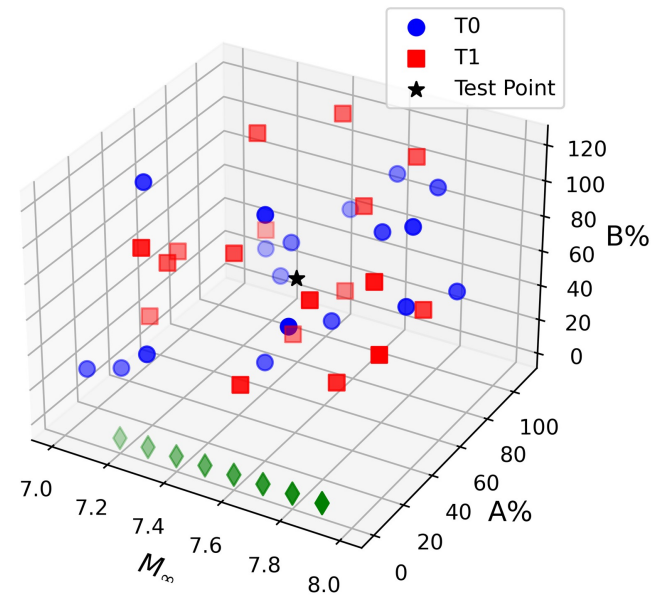


# Stage 1, 1/2: Sampling inputs & parameters



D0 Parameter Space

D1 Parameter Space



Deformation:  $y_w^i(x) = Ay_{wDi}(x)$

Wall temperature:  $T_w^i(x) = T_{ref} + BT_d^i(x)$

# Stage 1, 2/2: DAE-Constrained Optimization

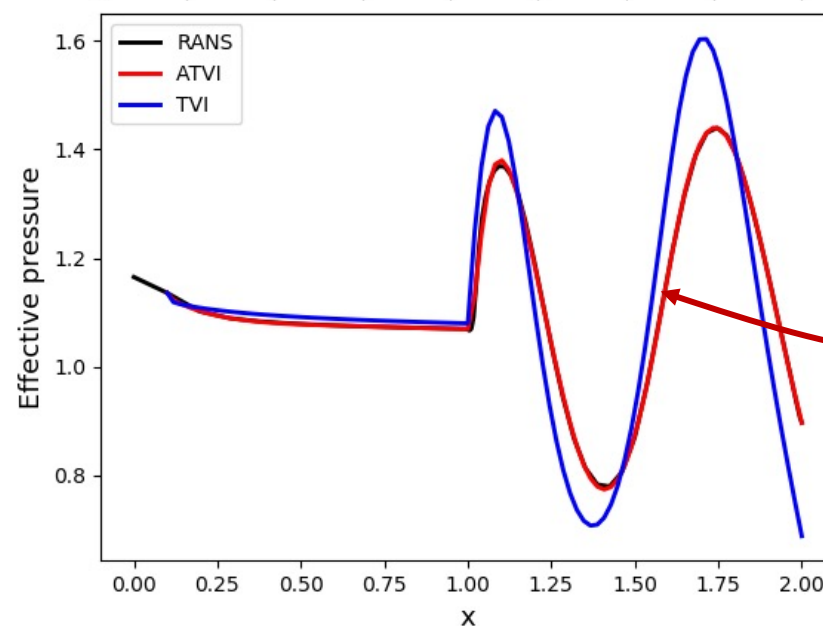
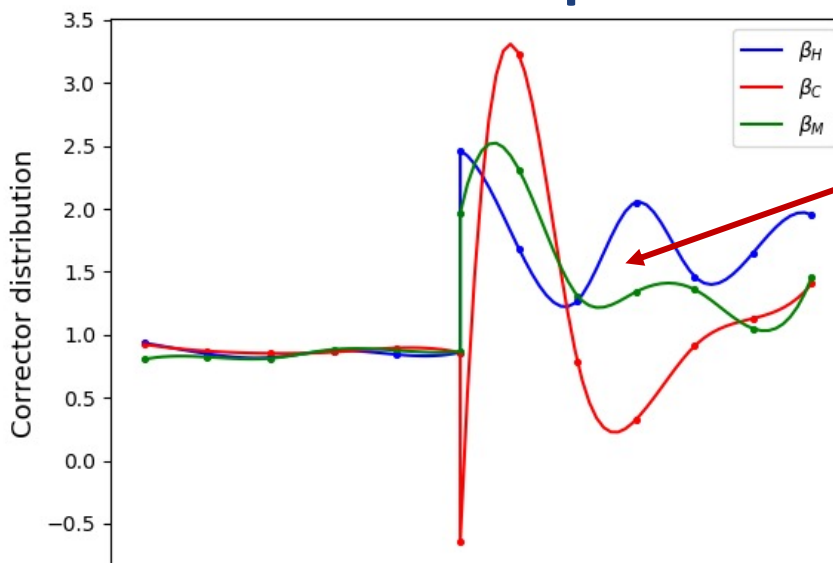
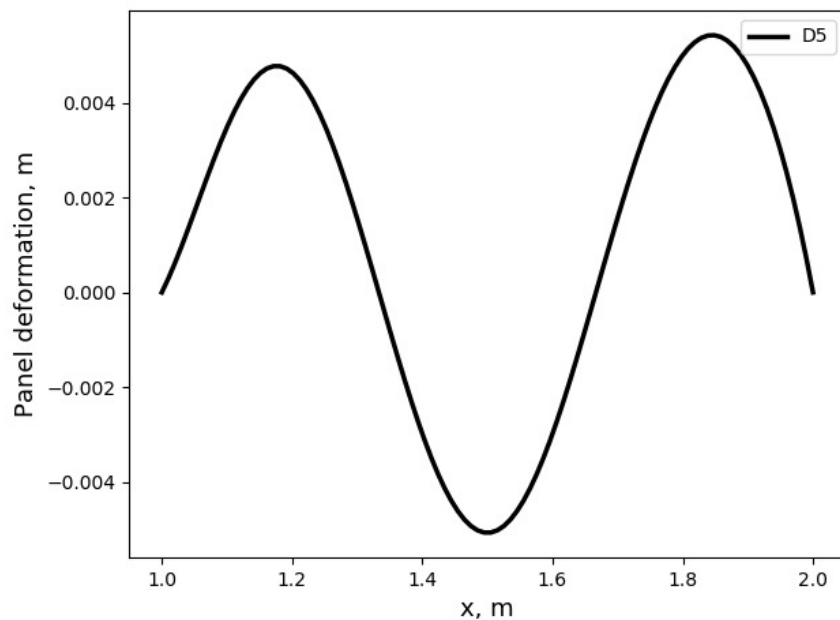
$$\mathbf{B}^i = \arg \min_{\mathbf{B}} J(\mathbf{z}_{RANS}^i, \mathbf{z}(\mathbf{B}))$$

$$s.t. \quad \mathbf{M}(\mathbf{y}, \mathbf{c}; \tau) \frac{d\mathbf{y}}{dx} = \mathbf{f}(\mathbf{y}, \mathbf{c}, x; \mathbf{u}, \tau)$$

$$\mathbf{c} = \beta_{spl}(x; \mathbf{B}) \odot \mathbf{g}(\mathbf{y}, x; \mathbf{u}, \tau)$$

$$\mathbf{z} = \mathbf{h}(\mathbf{y}, \mathbf{c}, x; \mathbf{u}, \tau)$$

Example: M76D5-100%

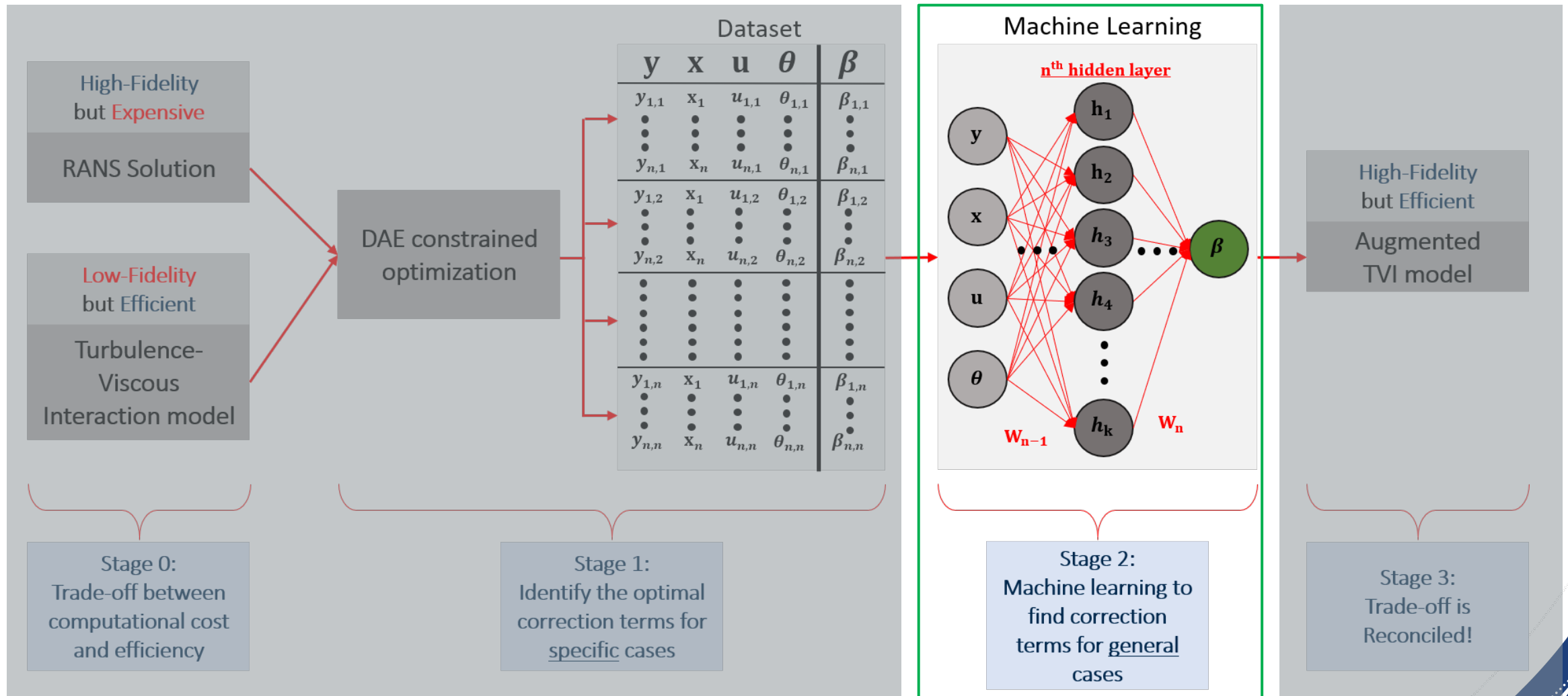


Training Dataset

$\mathbf{y}$	$\mathbf{x}$	$\mathbf{u}$	$\boldsymbol{\theta}$	$\boldsymbol{\beta}$
$y_{1,1}$	$x_1$	$u_{1,1}$	$\theta_{1,1}$	$\beta_{1,1}$
$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$
$y_{n,1}$	$x_n$	$u_{n,1}$	$\theta_{n,1}$	$\beta_{n,1}$
$y_{1,2}$	$x_1$	$u_{1,2}$	$\theta_{1,2}$	$\beta_{1,2}$
$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$
$y_{n,2}$	$x_n$	$u_{n,2}$	$\theta_{n,2}$	$\beta_{n,2}$
$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$
$y_{1,n}$	$x_1$	$u_{1,n}$	$\theta_{1,n}$	$\beta_{1,n}$
$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$
$y_{n,n}$	$x_n$	$u_{n,n}$	$\theta_{n,n}$	$\beta_{n,n}$



# Stage 2: Functional Representation of Correctors



# Stage 2: Machine Learning

## Gaussian Process Regression (GPR)

Training Dataset

$y$	$x$	$u$	$\theta$	$\beta$
$y_{1,1}$	$x_1$	$u_{1,1}$	$\theta_{1,1}$	$\beta_{1,1}$
$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$
$y_{n,1}$	$x_n$	$u_{n,1}$	$\theta_{n,1}$	$\beta_{n,1}$
$y_{1,2}$	$x_1$	$u_{1,2}$	$\theta_{1,2}$	$\beta_{1,2}$
$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$
$y_{n,2}$	$x_n$	$u_{n,2}$	$\theta_{n,2}$	$\beta_{n,2}$
$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$
$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$
$y_{1,n}$	$x_1$	$u_{1,n}$	$\theta_{1,n}$	$\beta_{1,n}$
$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$
$y_{n,n}$	$x_n$	$u_{n,n}$	$\theta_{n,n}$	$\beta_{n,n}$

$\mathbf{x}^*$ : new input,  $\mathbf{x}$ : training data point

$$\mathbf{y} \sim \text{GP}(\mathbf{m}(\mathbf{x}), k(\mathbf{x}, \mathbf{x}'))$$

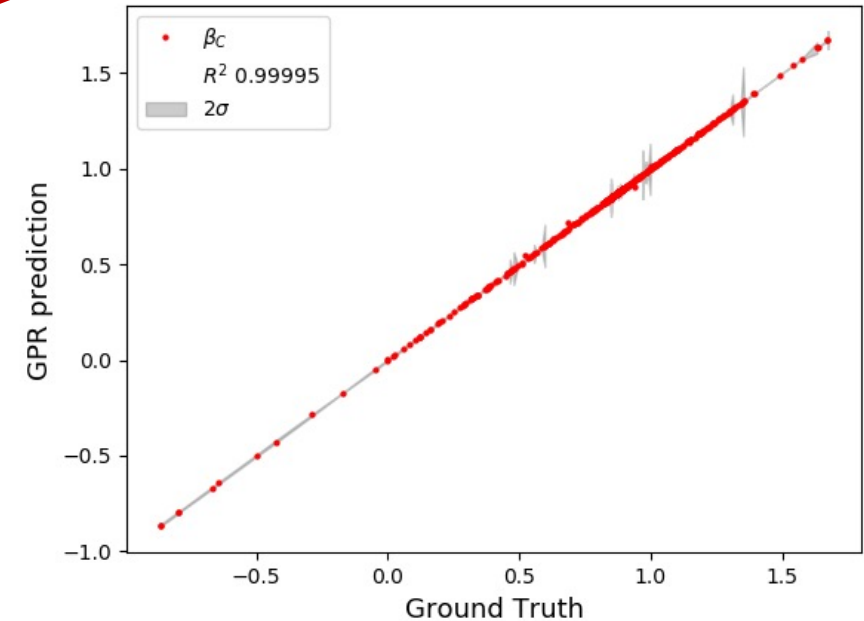
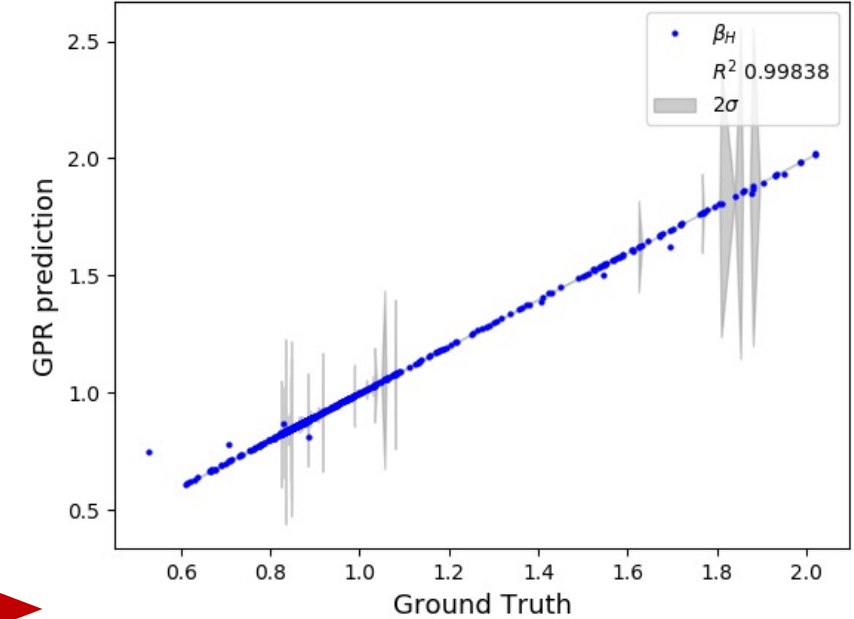
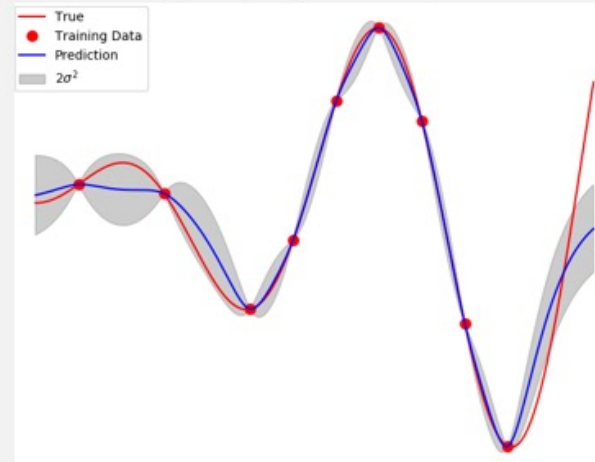
$$\mathbf{y}_{\text{GPR}} = N(\boldsymbol{\mu}(\mathbf{x}^*), \boldsymbol{\sigma}^2(\mathbf{x}^*))$$

→ Gaussian distribution

$$\boldsymbol{\mu}(\mathbf{x}^*) = \mathbf{k}(\mathbf{x}^*)^T \mathbf{K}^{-1} \mathbf{y}$$

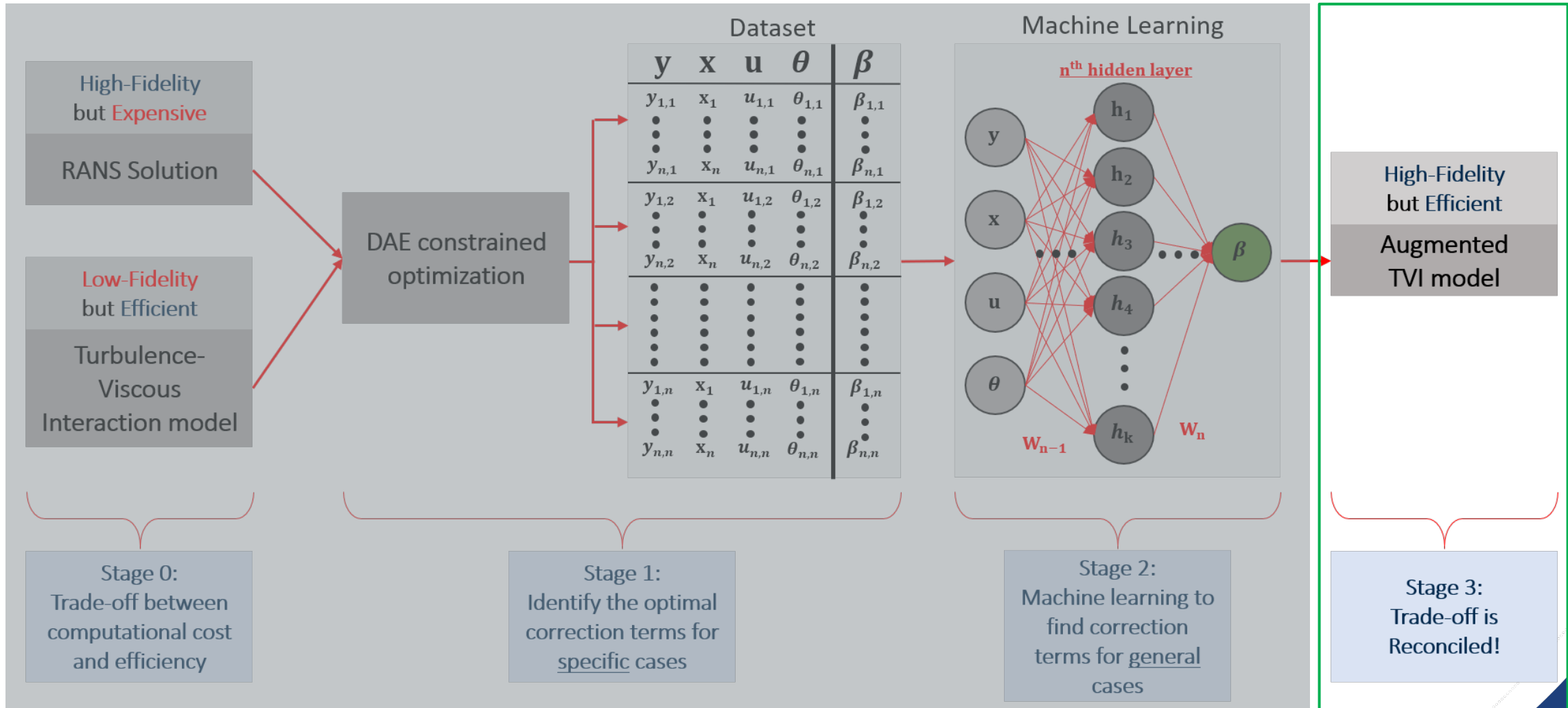
$$\boldsymbol{\sigma}^2(\mathbf{x}^*) = k(\mathbf{x}^*, \mathbf{x}) - \mathbf{k}(\mathbf{x}^*)^T \mathbf{K}^{-1} \mathbf{k}(\mathbf{x}^*)$$

$$\beta = \beta(y, x, u, \theta)$$



Going fancier, we could use tools like symbolic regression to get analytical expressions for the correction terms!

# Stage 3: Reconciling Trade-off

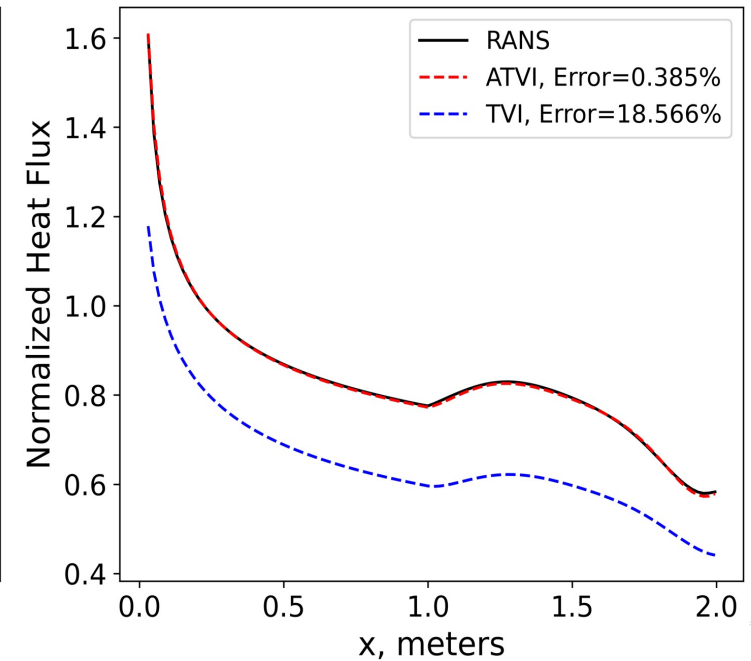
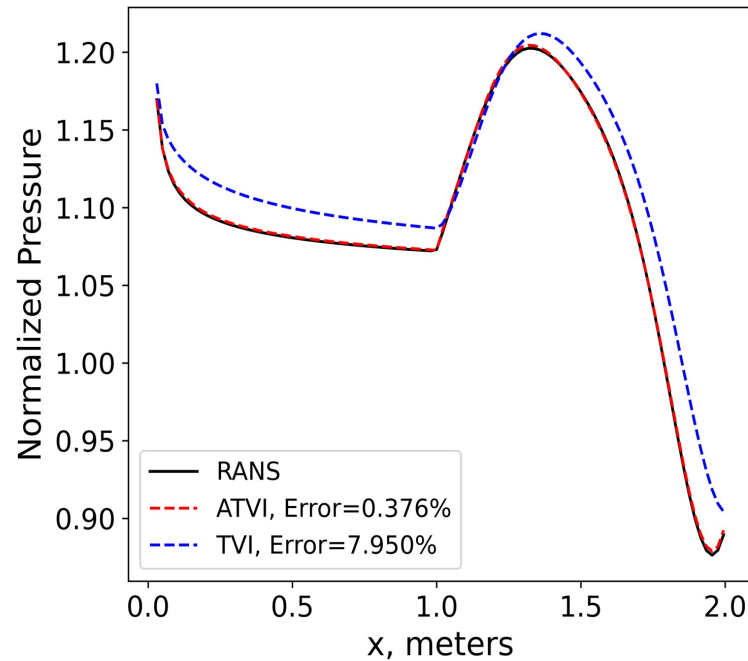
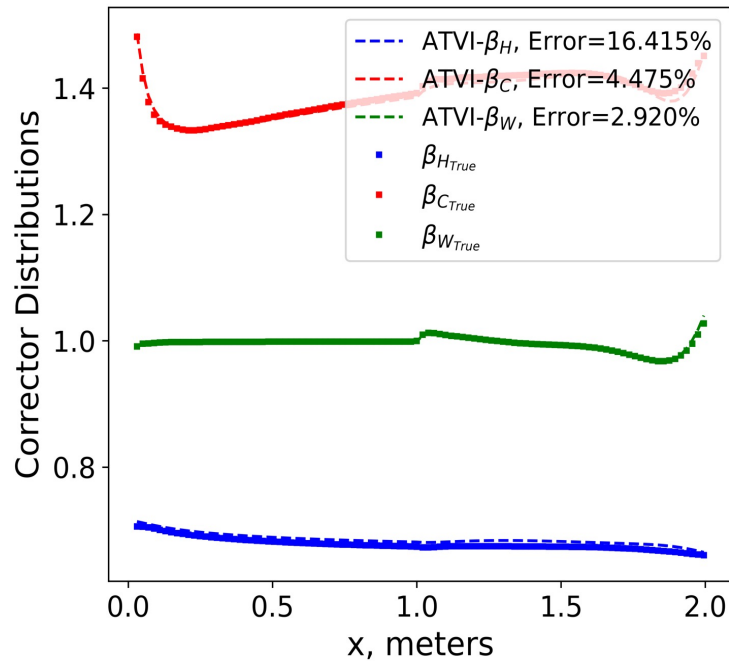


# Demo: New response, New flow conditions

Displacement:  $y_w(x) = 0.6[y_w^0(x) + y_w^1(x)]/2$

Wall temperature:  $T_w(x) = T_{ref} + 0.7[T_w^0(x) + T_w^1(x)]/2$

Mach number:  $M = 7.5$

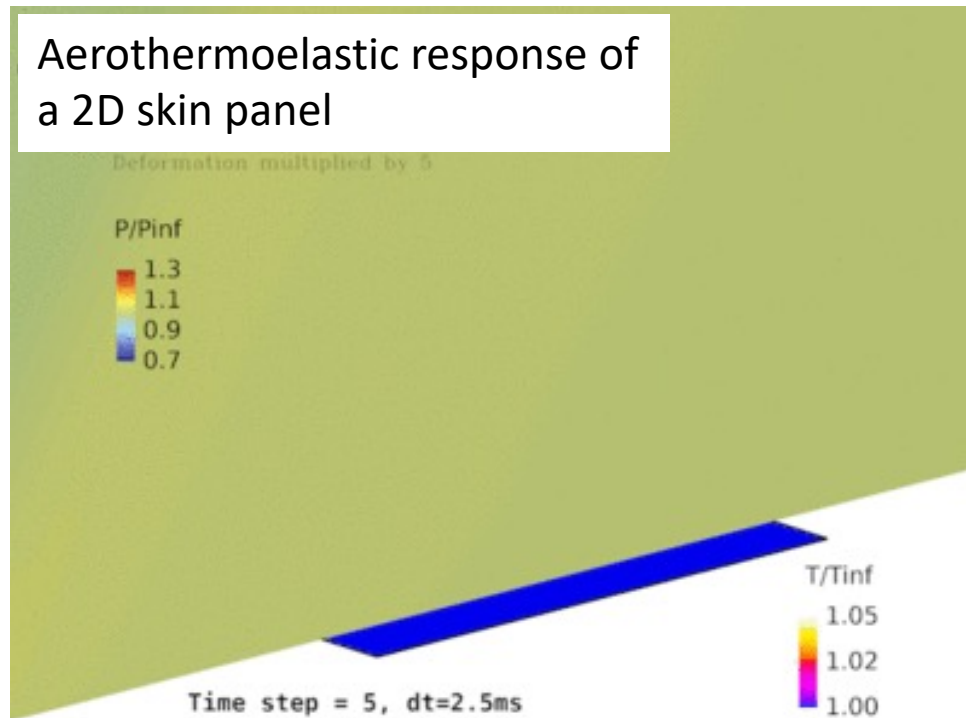


# Application

Back to Hypersonic Aerothermoelasticity

# Benchmark case for aerothermoelasticity

Aerothermoelastic response of a 2D skin panel



Name	$M_{\infty}$	$P_{\infty}$ (Pa)	$T_{\infty}$ (K)	Leading edge BC	Trailing edge BC
M7.523CP	7.523	3759.678	466.200	Clamped	Pinned
M7.750CC	7.750	3802.521	452.500	Clamped	Clamped
M7.400SS	7.400	3473.935	390.942	Pinned	Pinned
M7.523CX	7.523	3759.678	466.200	Clamped	Spring
M7.400XS	7.400	3473.935	390.942	Spring	Pinned

# HYPATE-X: **HYP**ersonic **AeroThermoElastic** e**Xtended**

## High Fidelity Models

- Time-Accurate Transient Analysis
- Long-Term Quasi Steady Analysis
- Linearized Stability Analysis

## Aerothermodynamics

Analytical Models  
Unsteady RANS  
Large Eddy Simulation

## Thermoelasticity

Galerkin-based/Finite-difference  
Geometrically Nonlinear Shell FEM  
Fully Nonlinear Solid FEM

## Rigid Body Dynamics

Euler-Lagrangian  
Dynamics

Multi-Fid. Gaussian Proc. Regr.  
Physics-Infused ROM

## Aero-Thermal-Acoustics

Linear Time-Varying Model for Tangent Subspace  
Sparse Learning for Model Refinement

## Servo-Thermoelasticity

## Reduced Order Models

- Tradeoff between Accuracy & Model Complexity
- Convex Optimization + Dynamic System Theory
- Parametric Sensitivity Analysis

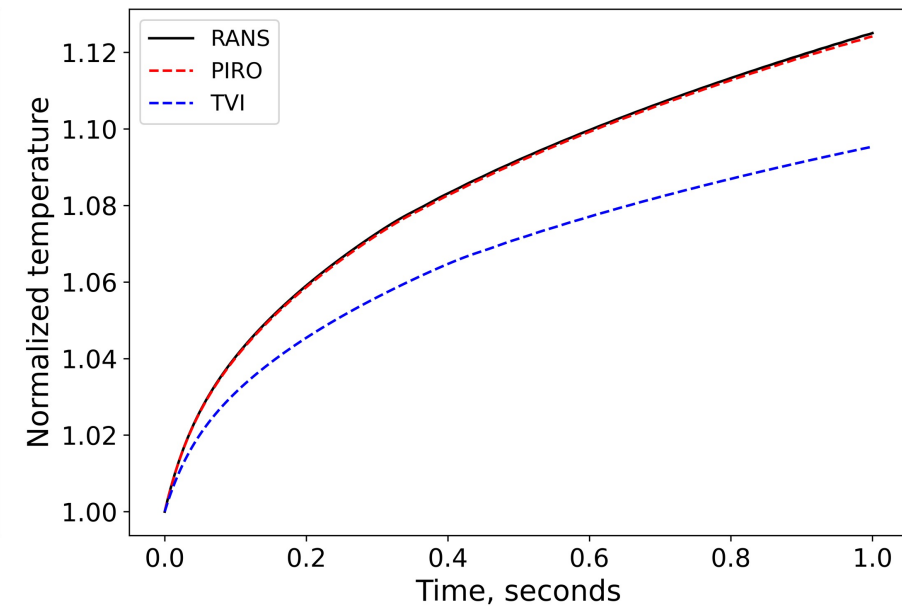
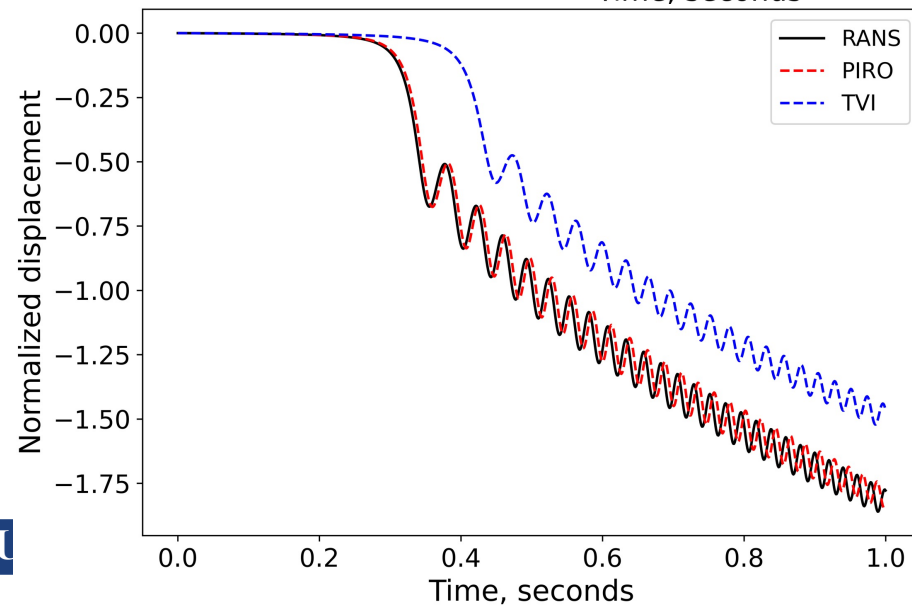
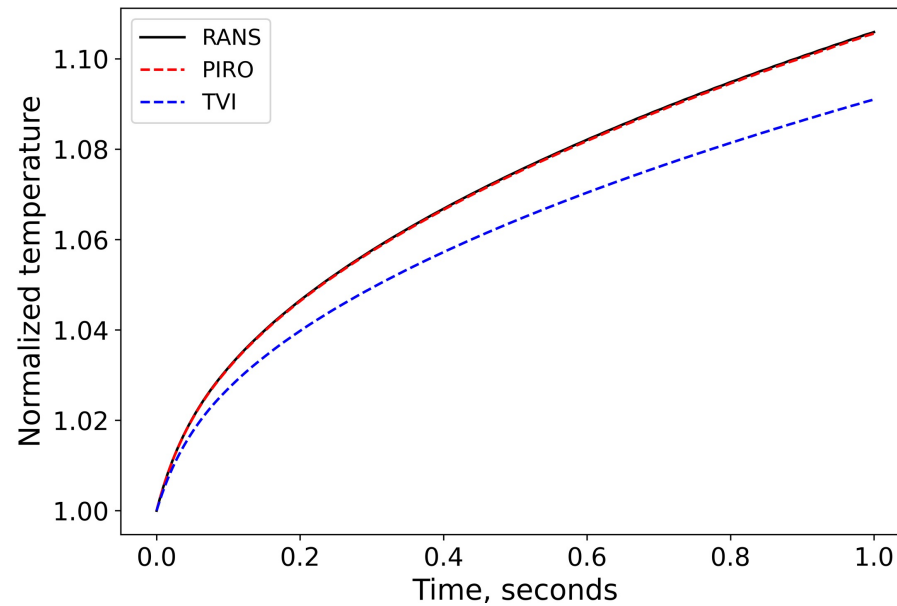
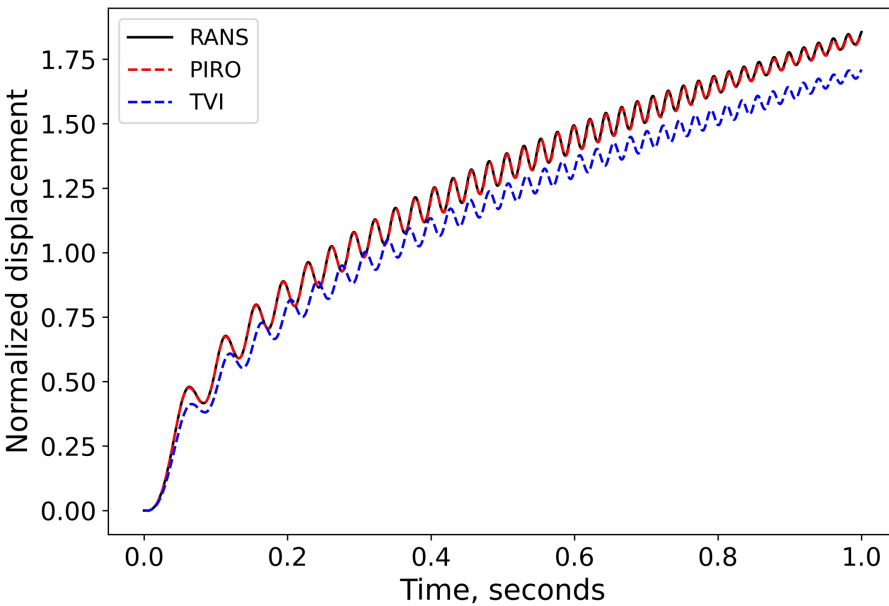
## Collaborators:

- Drs. P.P. Friedmann and T. Rokita (UMich)
- Drs. P. Singla and X.I.A. Yang (PSU)
- Dr. K.M. Hanquist (UofAz)

Existing  
modules

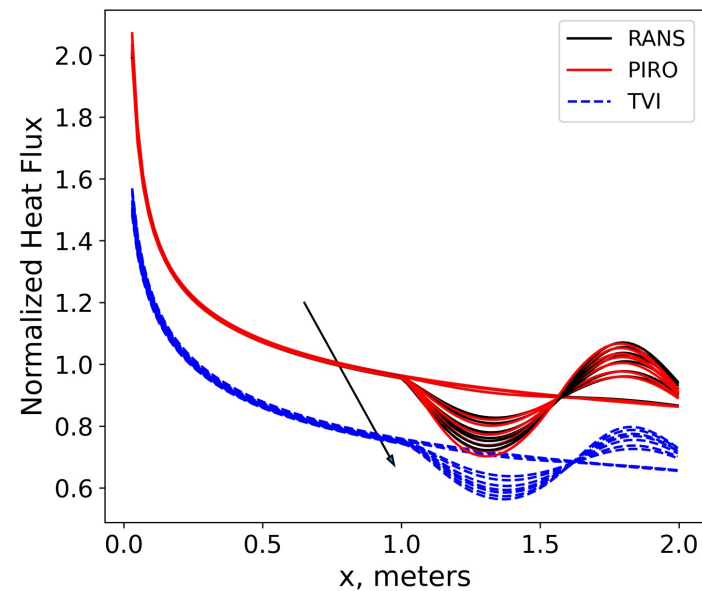
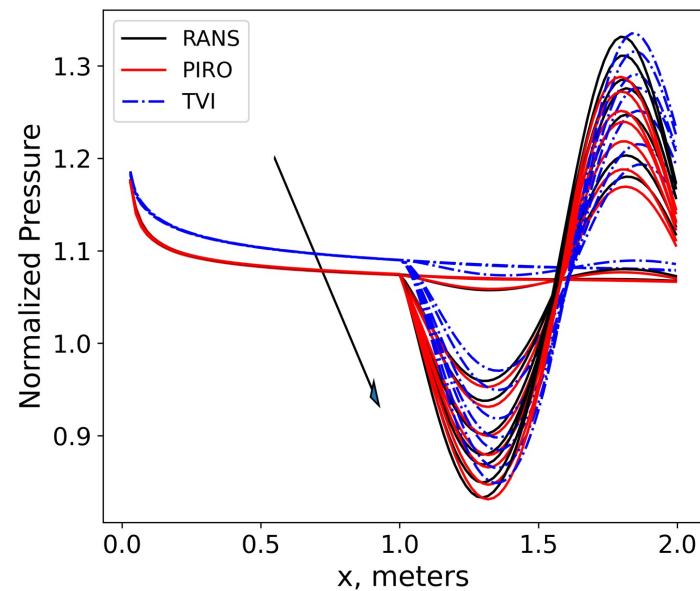
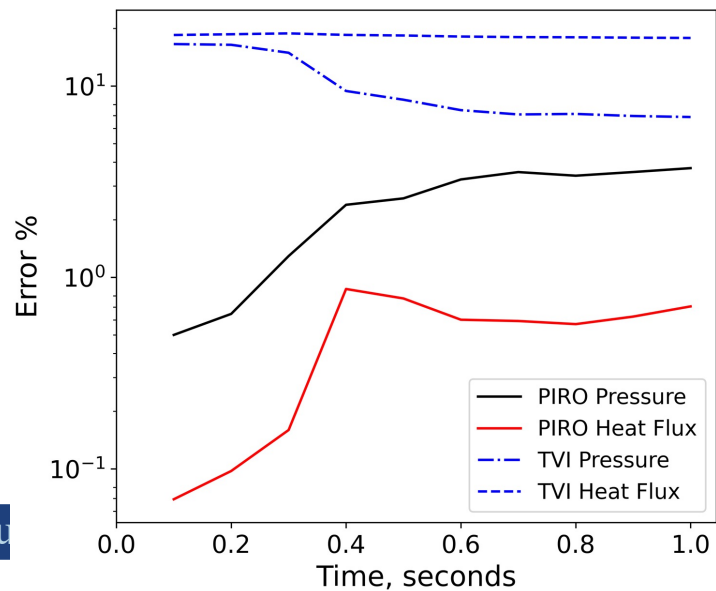
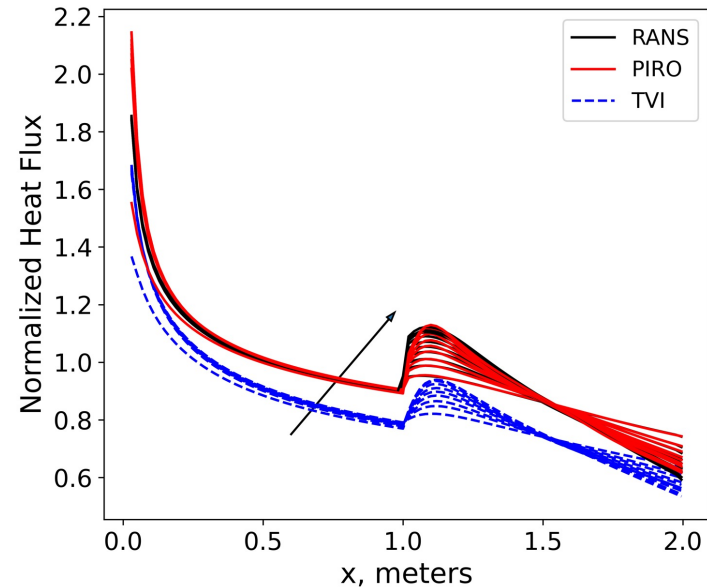
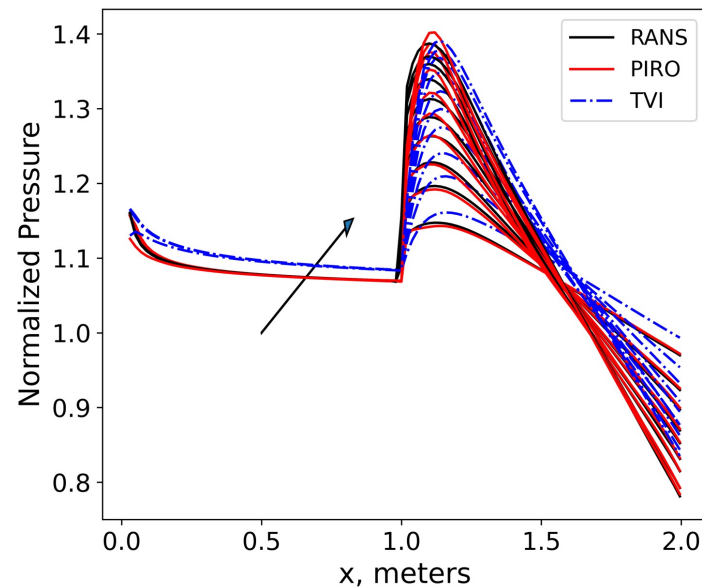
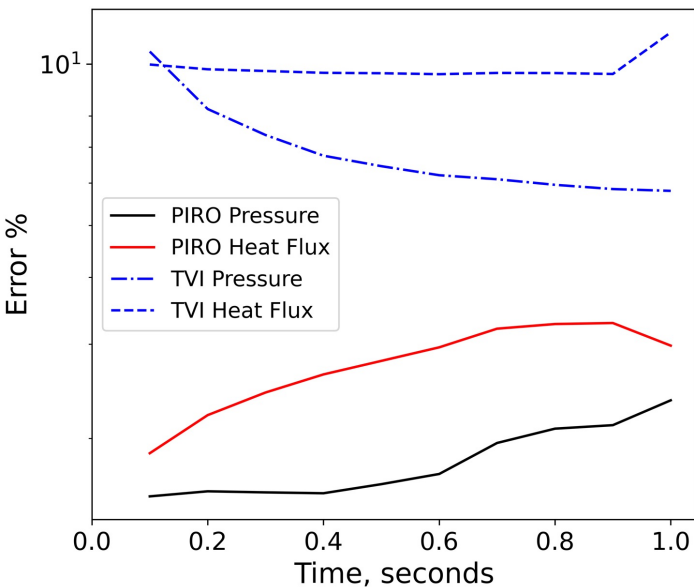
Developing  
modules

# Accuracy of RANS at cost of milli-secs

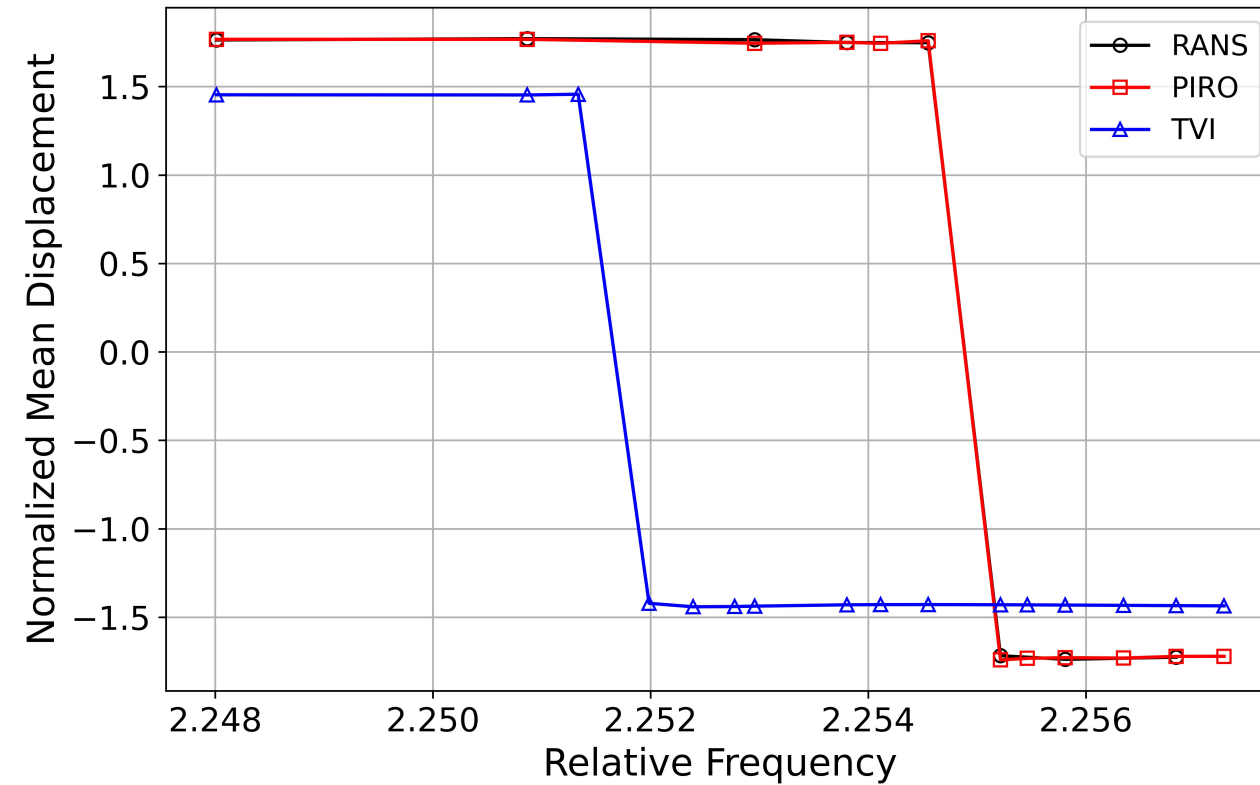
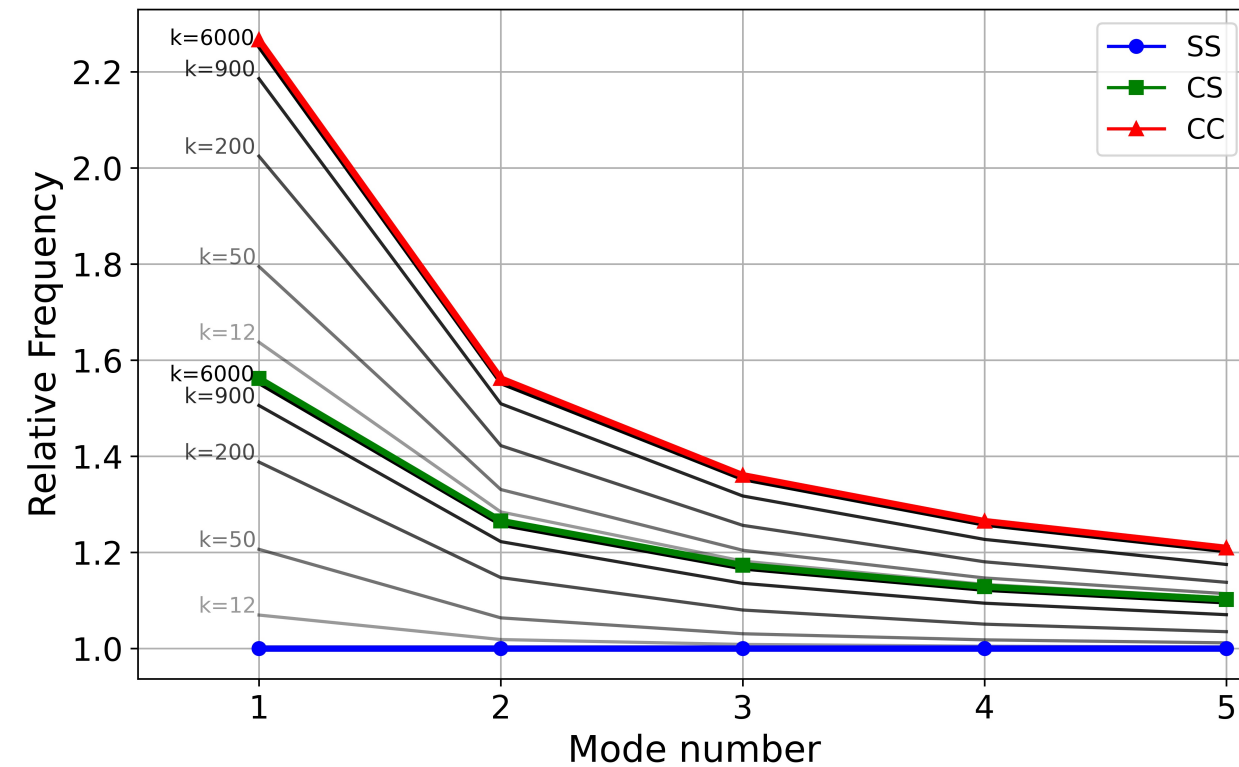




# A closer look at the responses



# Enabling parametric study as well



# Key takeaways

## Summary:

- Presented the formulation of Physics-Infused Reduced-Order Modeling.
- Demonstrated the methodology for a hypersonic aerothermodynamic application.
- Comparing to conventional aerothermal surrogate:
  - ❑ Generalize well to operating conditions and thermoelastic responses not in the training data set.
  - ❑ Requires  $<10^2$  samples for any response, v.s.  $10^3$ - $10^4$  samples → Much less samples
  - ❑ Computational cost 90 ms, v.s. 50 ms → Similar computational efficiency

## Future Work:

- Extend the methodology for general DAE problems – Open to collaborations!
- Develop a general framework for systematic creation of physics-infused ROM.
- Couple to frameworks of multi-disciplinary optimization.

# Thank you!

## Questions?

Contact: [daning@psu.edu](mailto:daning@psu.edu)  
Lab website: [apus.psu.edu](http://apus.psu.edu)